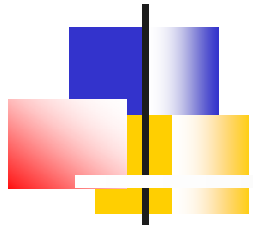


Isochronous Ring at RIKEN



I. Arai, T. Komatsubara, A. Ozawa, K. Sasa, Y. Yasuda (*University of Tsukuba*)
M. Fujinawa, Y. Fukunishi, A. Goto, T. Ohnishi, H. Okuno, H. Takeda,
M. Wakasugi, M. Yamaguchi, Y. Yamaguchi, Y. Yano (*RIKEN*)
T. Kikuchi (*Utsunomiya University*)
T. Suzuki, T. Yamaguchi (*Saitama University*)
T. Ohtsubo (*Niigata University*)



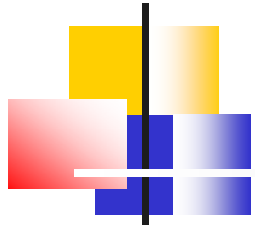
Objective

➤ to Establish

A New Scheme of
Precise Mass Measurement

➤ For Energetic RI Beam
From RIBF at RIKEN

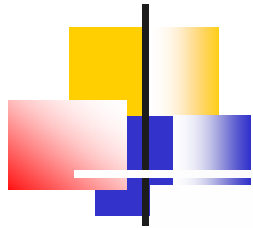
200 A MeV, $m/q \sim 3.0$



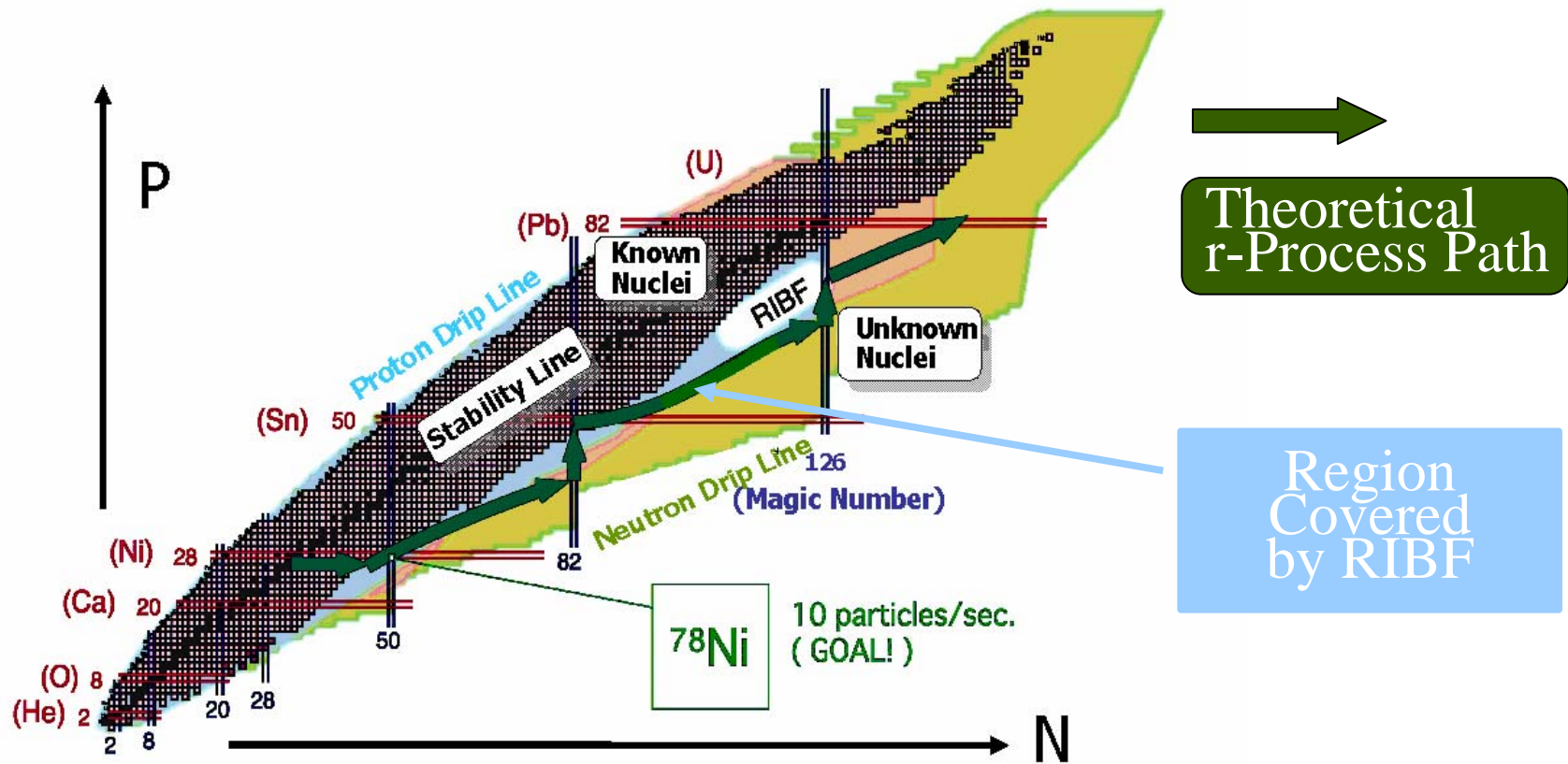
Physical Interests

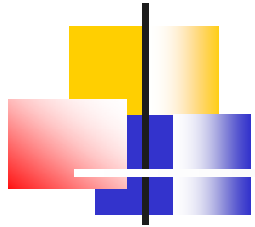
to Study

- Nuclei Far from Stability
 - ✓ "Exotic" Nuclear Structure
- Astrophysical r-Process Path
 - ✓ Super Nova Nucleo-Syntheses



Nuclei Far from stability





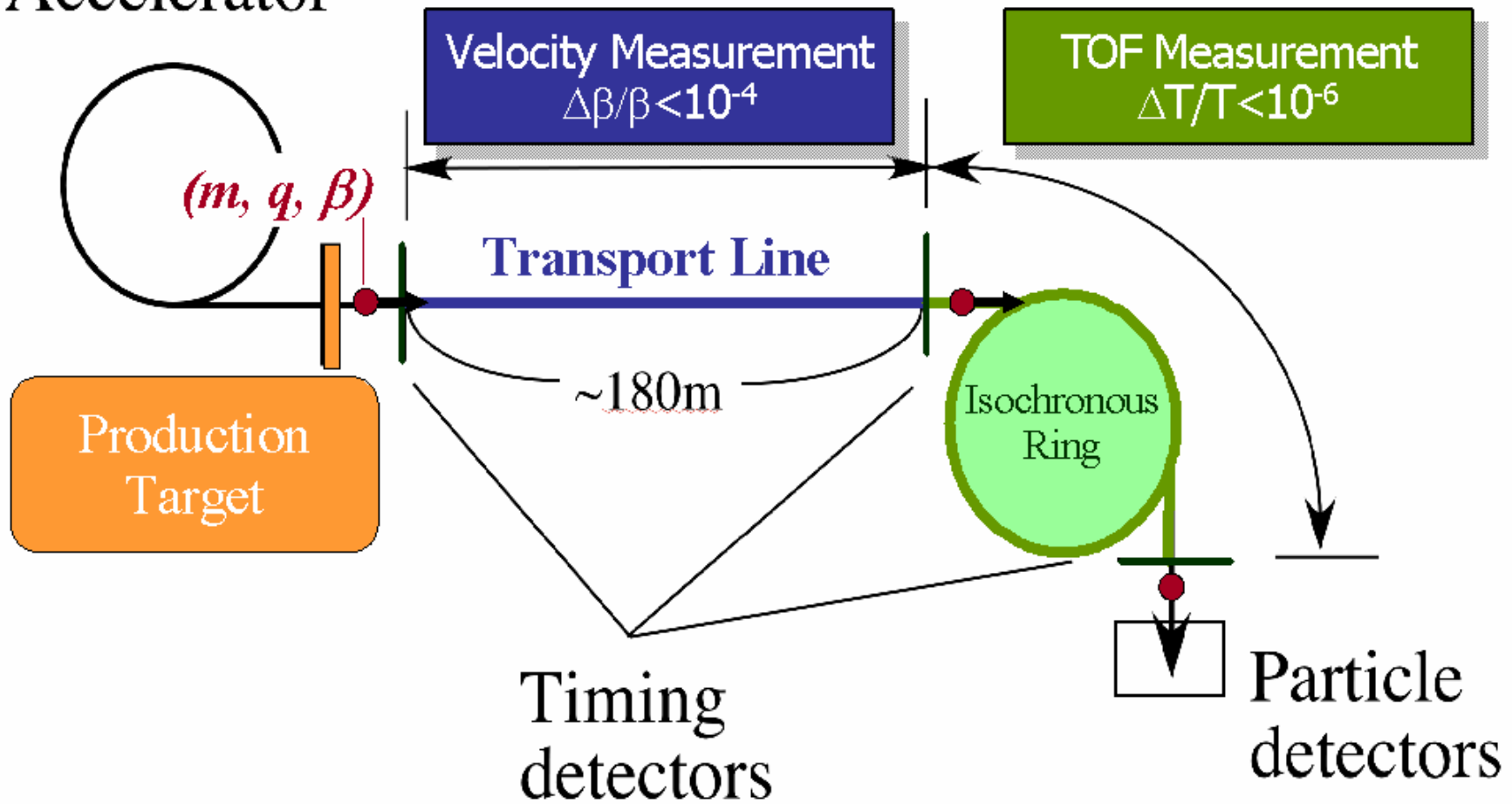
What is New Scheme ?

Combination of

- Velocity Measurement
in Transport Line
- TOF Measurement
in Isochronous Ring

Proposed Apparatus

Accelerator





Principle of Mass Measurement

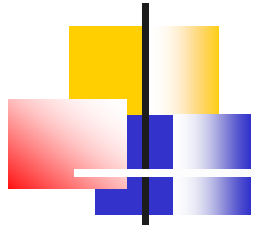
➤ For Known Nucleus, $T_0 = 2\pi \frac{m_0 \gamma_0}{qB}$
 T_0, m_0, q, γ_0 : *Fixed*

➤ For Unknown Nucleus, $T_1 = 2\pi \frac{m_1 \gamma_1}{qB}$
 T_1, γ_1 : *Measured*

➤ Then, m_1 : *Determined*

$$\frac{m_1}{q} = \left(\frac{m_0}{q}\right) \frac{T_1 \gamma_0}{T_0 \gamma_1} = \left(\frac{m_0}{q}\right) \frac{T_1}{T_0} \sqrt{\frac{1 - \beta_1^2}{1 - \left(\frac{T_1}{T_0} \beta_1\right)^2}}$$

$$\gamma = \frac{1}{\sqrt{1 - \beta^2}}$$



Accuracy of Measurement

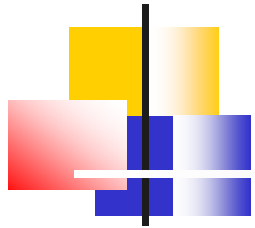
➤ Expected Accuracy for Mass

$$\left(\frac{\delta m_1}{m_1}\right)^2 = \left(\frac{\delta T_1}{T_1}\right)^2 + \underbrace{\left(\frac{2\beta_1^2}{(1-\beta_1^2)^2} \frac{T_1 - T_0}{T_0}\right)}_{\sim 10^{-4}} \left(\frac{\delta\beta_1}{\beta_1}\right)^2$$

➤ Mass Resolution of $\sim 10^{-6}$ is Achieved under Feasible Condition

$\sim 10^{-4}$
for $\sim 1\%$ *TOF*
Difference

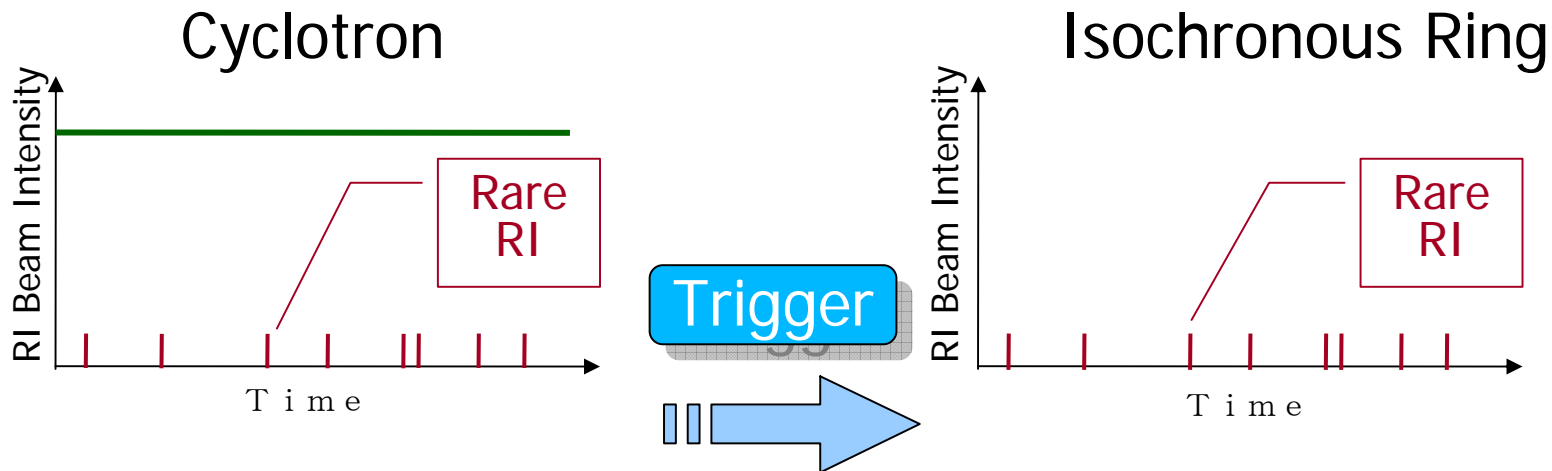
$$\frac{\delta T_1}{T_1} \sim 10^{-6}, \quad \frac{\delta\beta_1}{\beta_1} \sim 10^{-4}$$

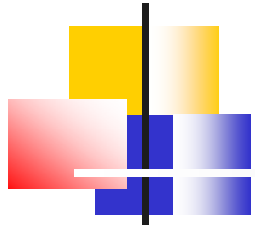


Individual Injection

Triggered Injection

- Sampling on Trigger
- Accepts Only Interested Particles
- 100% Efficiency in Principle



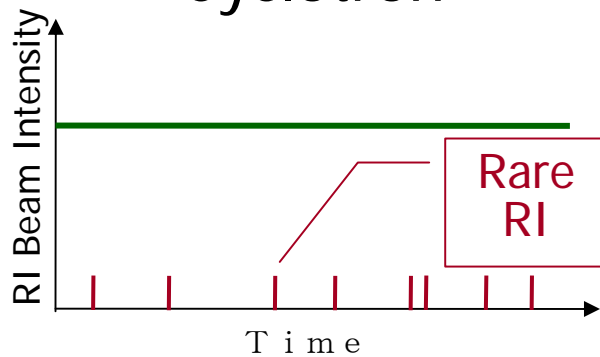


Conventional Method

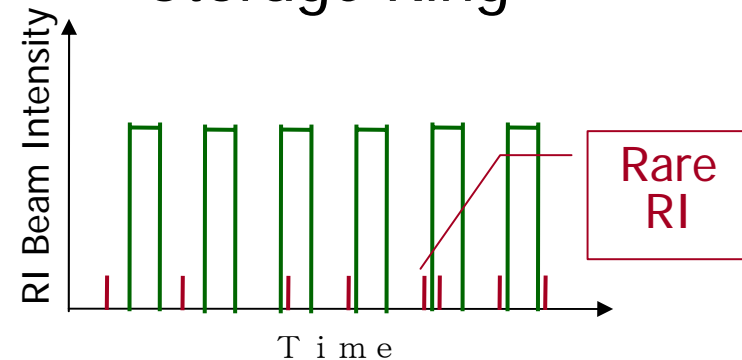
Cyclic Injection

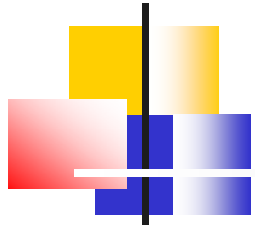
- Sampling of Beam Particles
Synchronized with Operation of
Storage Ring
- Low Efficiency

Cyclotron



Storage Ring



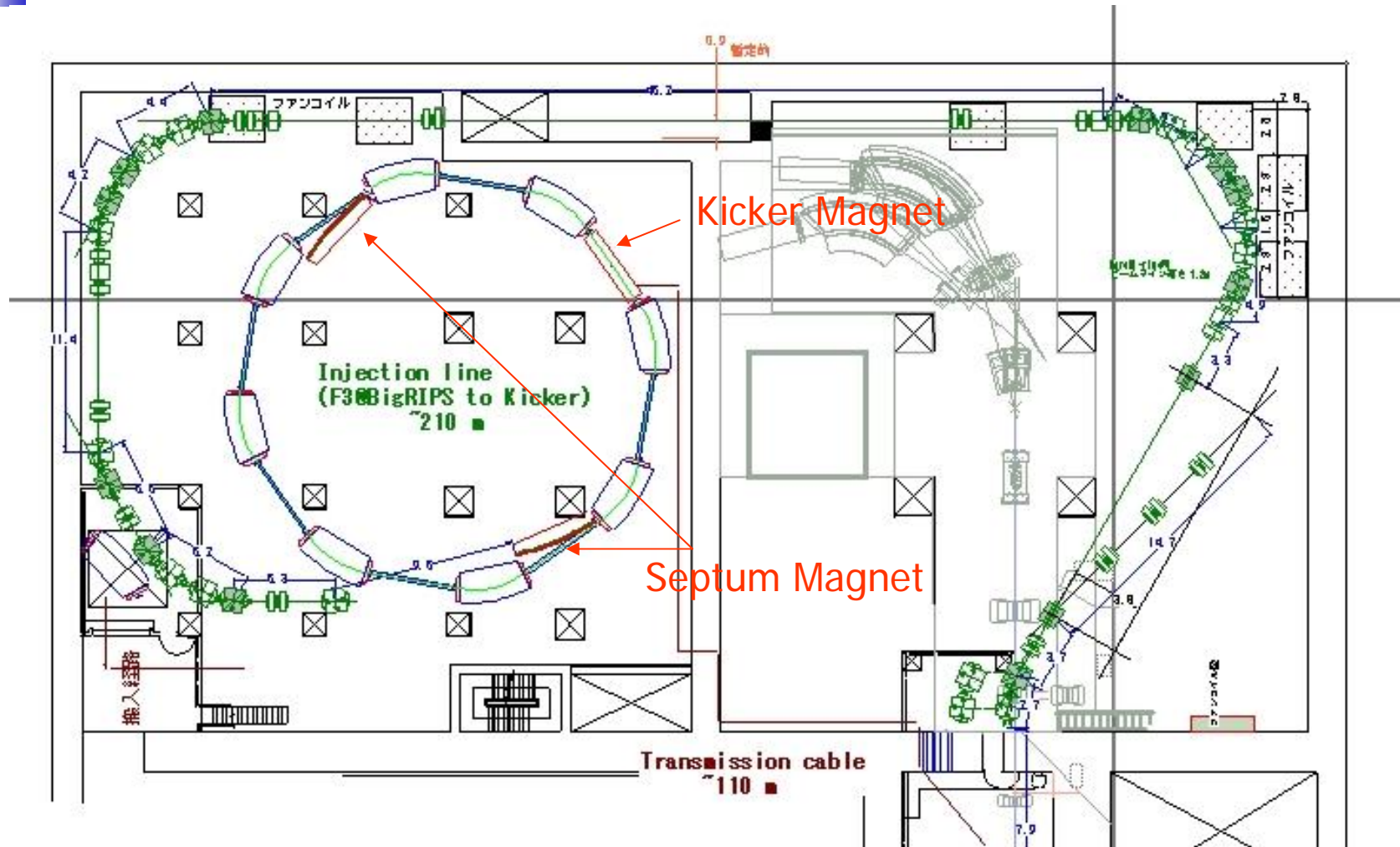


Dead Time/Maximum Rate

- Dead Time $\sim 400 \mu\text{sec}$
 - ✓ Beam Transport
 - ✓ for 1,000 turns Circulation in Isochronous Ring

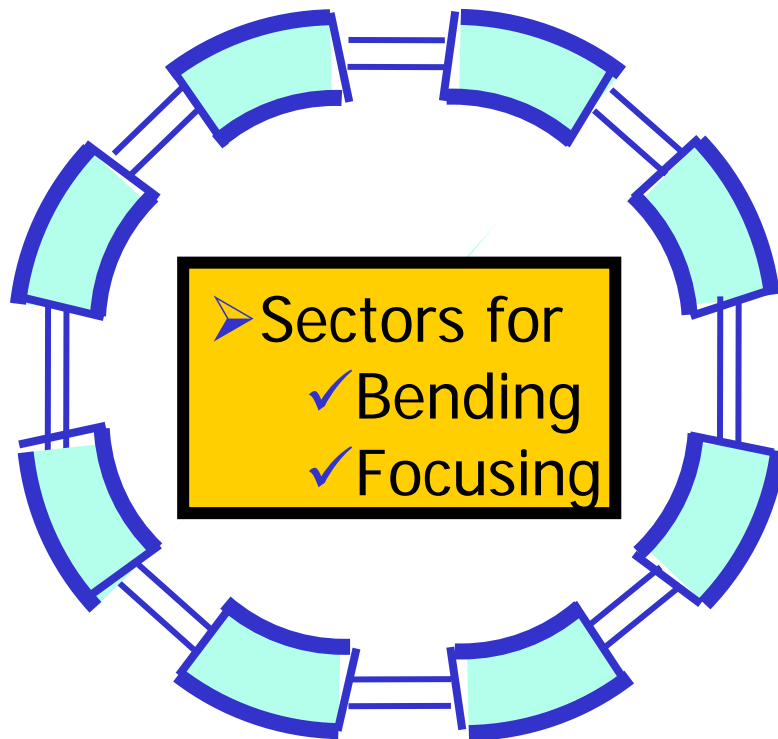
➡ $\sim 2,500 \text{ particles /sec at max.}$
- Expected Rate of Rare RI around ^{78}Ni
 $\sim 10 \text{ particles/sec}$

Layout of Experimental Apparatus at RIBF (Plan View)





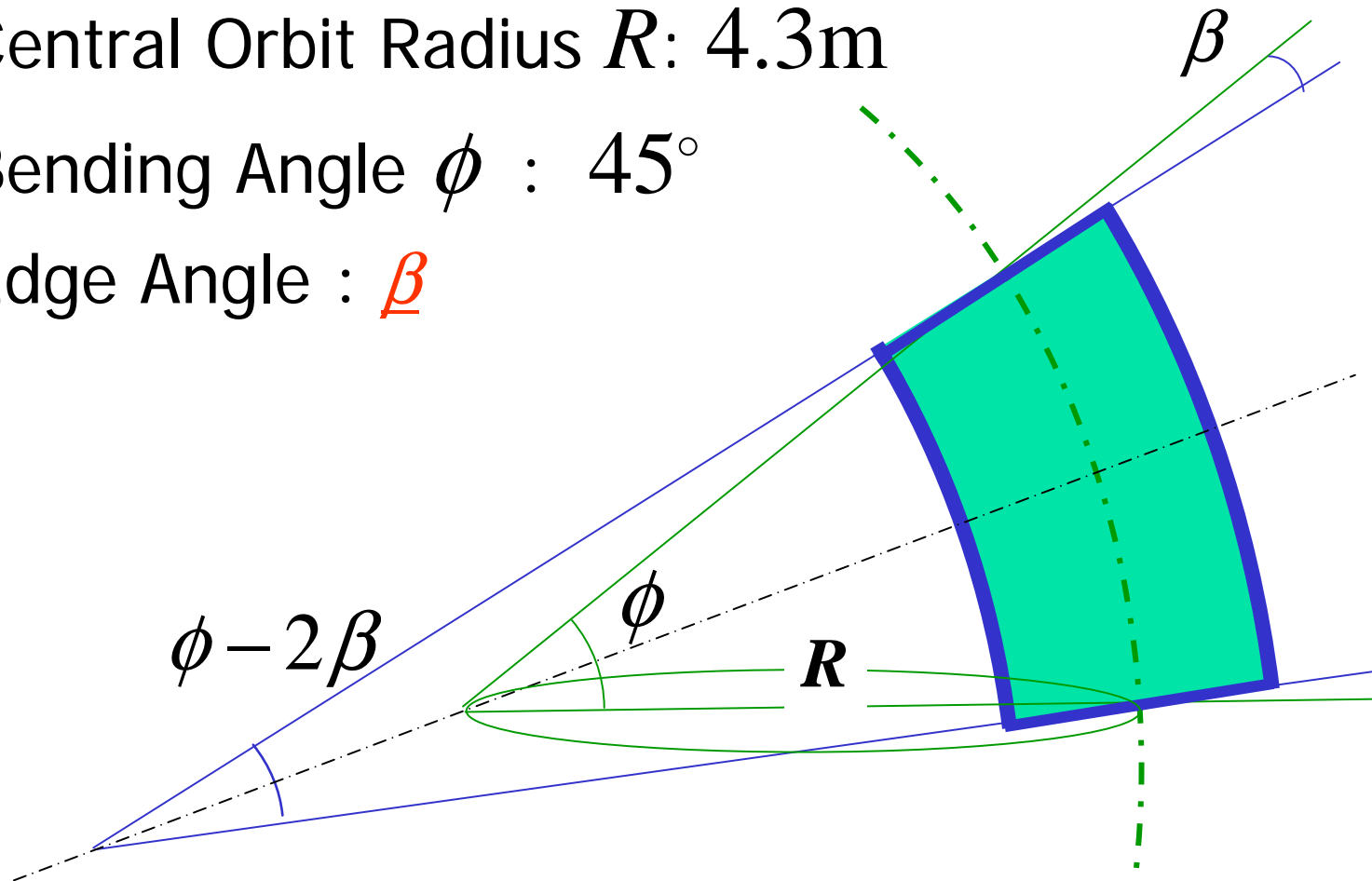
Configuration

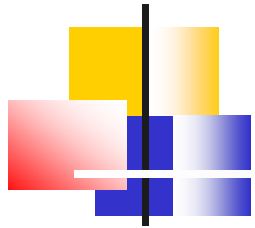


- Separate Sector Ring:
 - ✓ 8 Sectors
 - ✓ 8 Straight Sections
- Circumference : 67.36 m
- Circulation : 1,000 Turns
- Isochronicity: $\frac{\Delta T}{T} \leq 10^{-6}$
- Momentum Range:
$$-0.01 \leq \frac{\Delta P}{P} \leq +0.01$$

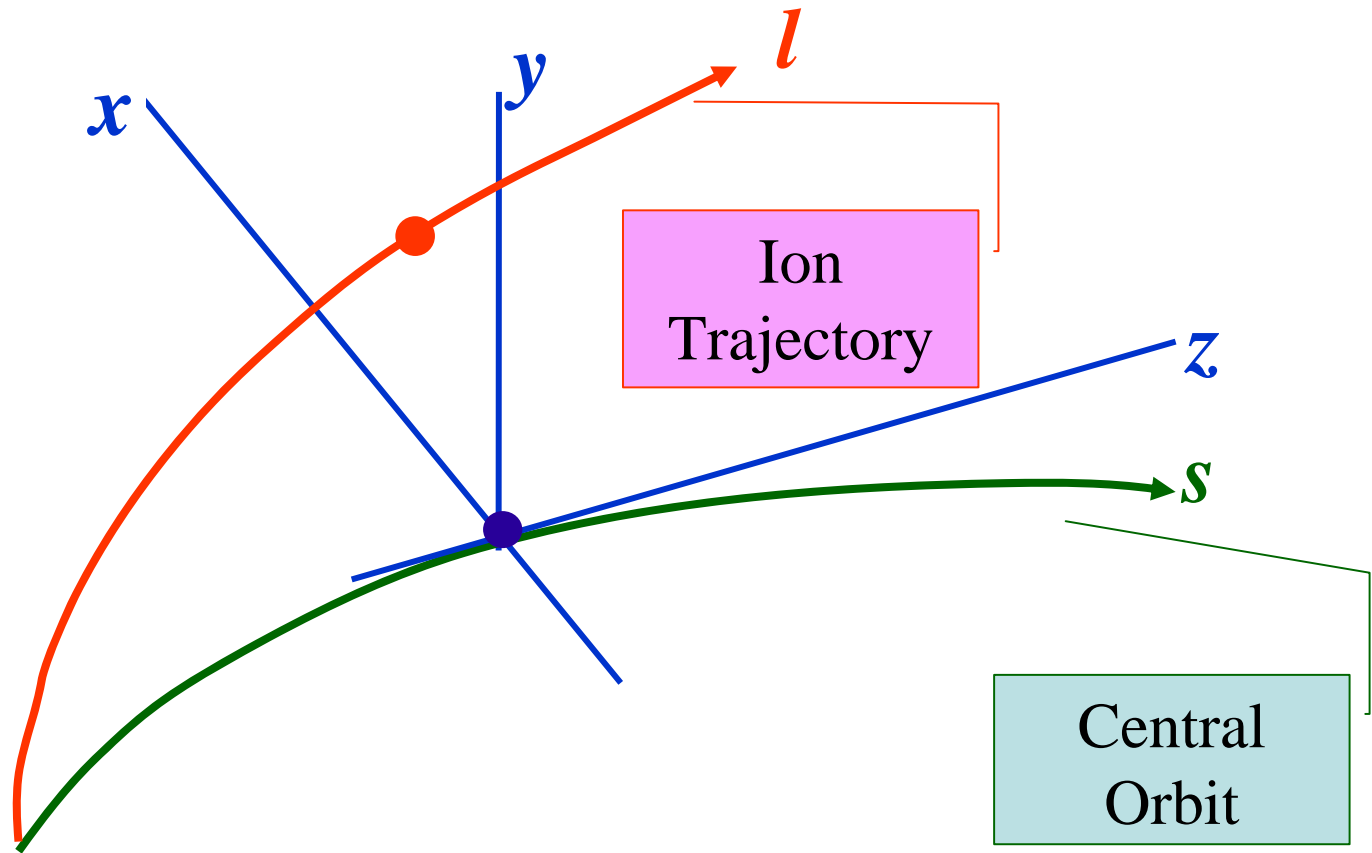
Flat-Edged Sector

- Central Orbit Radius R : 4.3m
- Bending Angle ϕ : 45°
- Edge Angle : β





Coordinate System





Edge Angle β

Needed for

➤ Vertical Focusing

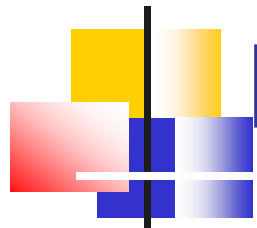
$$\Delta y' = -\tan \beta \times \frac{y}{R\gamma}$$

(in Hard Edge Approx.)

➤ Horizontal Tune

✓ Designed Value is

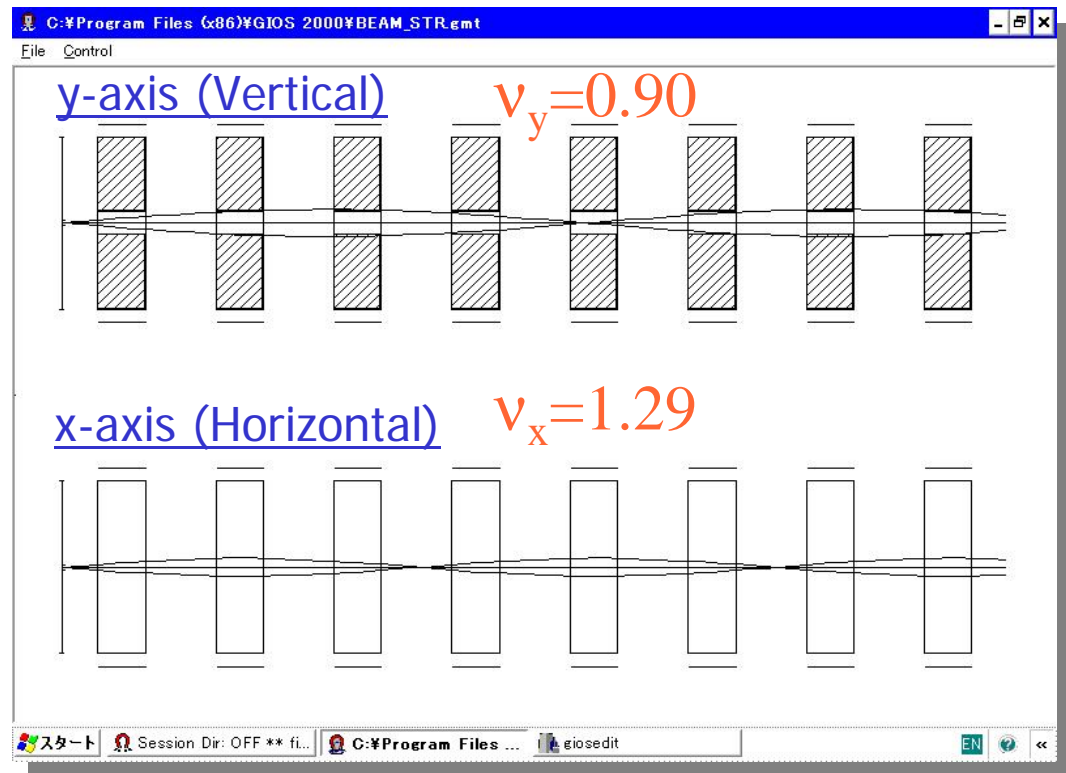
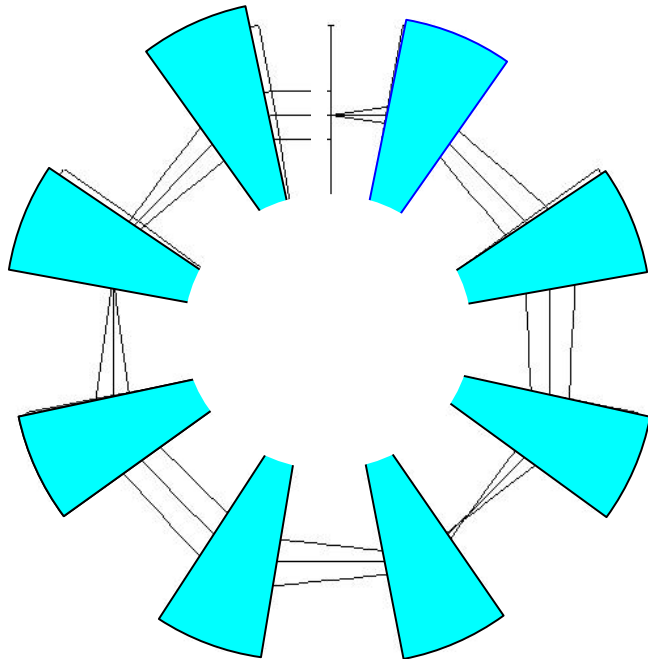
$$\nu_y \approx 0.9$$



Edge Angle for $v_y=0.9$

with Use of GIOS Simulator

$$\beta = 7.6^\circ$$



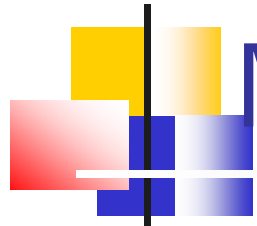


Isochronicity

Keep the Same TOF for Particles
with Different Momenta by

- Applying Non-Uniform Magnetic Field
 - ✓ Shifts the Trajectory along x-Axis
 - ✓ Changes the Curvature of Trajectory

Both result the Change of Path Length

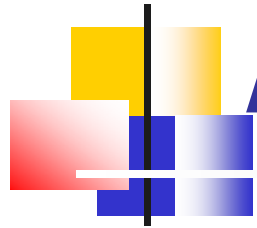


Magnetic Field

Combination of

- Main Field: B_0
Giving a Storage Force
- Trim Field: $B_T(x)$
Keeping an Isochronicity

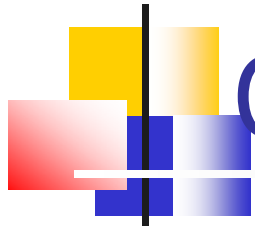
$$B_T(x) = B_0(Ax + Bx^2)$$



Adjusting of Trim Field

- Step1: First Order Solution in $\Delta p/p$
 - ✓ Obtained under 1) Geometrical Relation and 2) Isochronicity Condition
 - ✓ Gives 1) Desirable Value of A and 2) Momentum Dispersion ξ

- Step2: Further Fine Tuning for A and Determination of Parameter B
 - ✓ By Hand
 - ✓ using Newly Developed Simulator



Geometrical Relation

$$\left\{ R + \delta - \left(1 + \frac{\Delta P}{P} - \varepsilon \right) R \right\} \tan \frac{\phi}{2}$$

$$R + \delta - \left(1 + \frac{\Delta P}{P} - \varepsilon \right) R$$

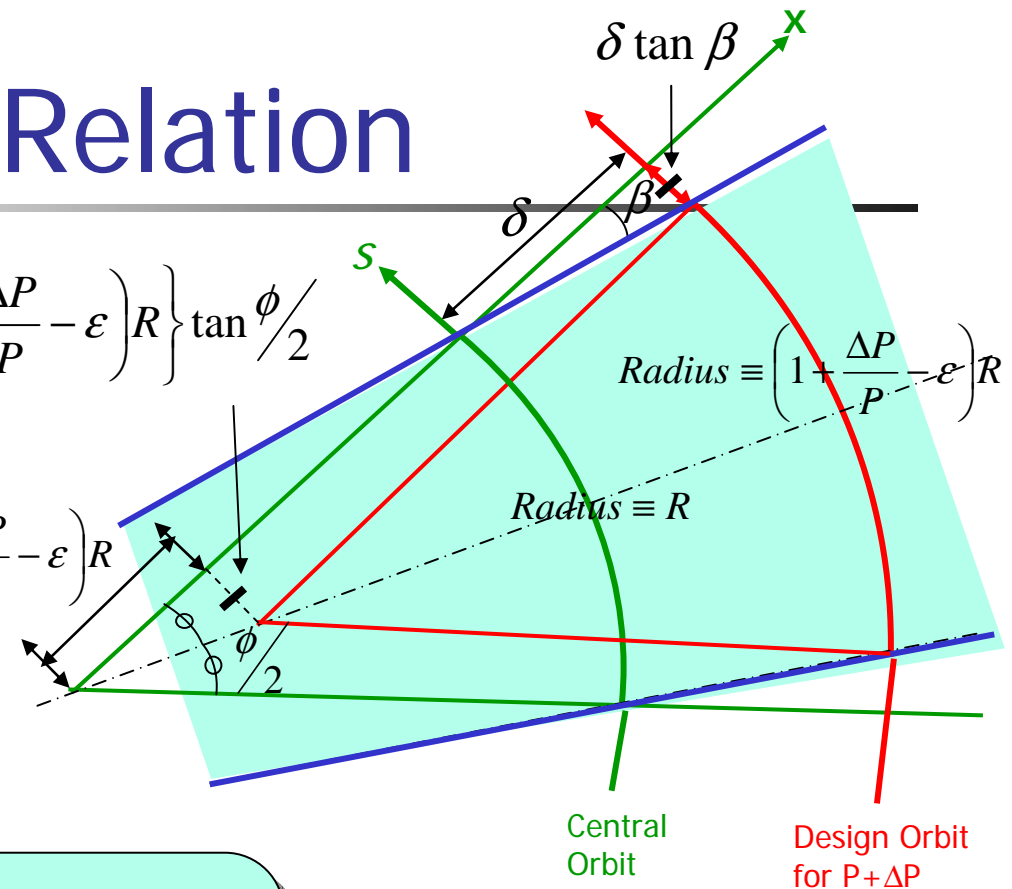
$$\text{Radius} \equiv \left(1 + \frac{\Delta P}{P} - \varepsilon \right) R$$

$$\text{Radius} \equiv R$$

Between δ and ε

$$\left\{ R + \delta - \left(1 + \frac{\Delta P}{P} - \varepsilon \right) R \right\} \tan \frac{\phi}{2} = \delta \tan \beta$$

ε : Fraction of Trim Field





Isochronicity Condition

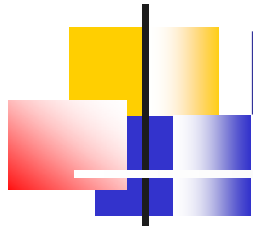
Same TOF among Different Momenta

$$\frac{(\gamma + \Delta\gamma) \left\{ R\phi \left(1 + \frac{\Delta P}{P} - \varepsilon \right) + S + 2\delta \tan \beta \right\}}{P + \Delta P} = \frac{\gamma(R\phi + S)}{P}$$

TOF of Design Orbit
for $p + \Delta p$

TOF of
Central
Orbit

for Single Unit Segment

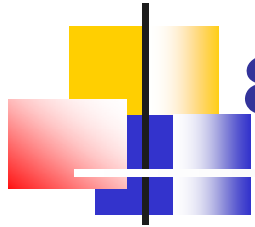


First Order Solution in $\Delta p/p$

$$\delta = \xi \frac{\Delta p}{p}, \quad \varepsilon = \left(1 - \frac{\xi \tan \frac{\phi}{2} - \tan \beta}{R \tan \frac{\phi}{2}} \right) \frac{\Delta P}{P}$$

ξ : Momentum Dispersion

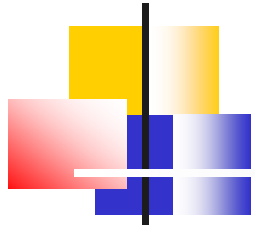
$$\begin{aligned} \xi &= \frac{\partial x}{\partial (\Delta P/P)} \\ &= \frac{\tan \frac{\phi}{2}}{\tan \frac{\phi}{2} - \tan \beta} \frac{\phi + S/R}{\phi + \frac{2 \tan \frac{\phi}{2} \tan \beta}{\tan \frac{\phi}{2} - \tan \beta}} \frac{1}{\gamma^2} R \end{aligned}$$



ε as a function of δ

Using δ/ξ in place of $\Delta P/P$

$$\begin{aligned}\varepsilon &= \left(1 - \frac{\xi \tan \frac{\phi}{2} - \tan \beta}{R \tan \frac{\phi}{2}} \right) \frac{\Delta P}{P} \\ &= \left(1 - \frac{\xi \tan \frac{\phi}{2} - \tan \beta}{R \tan \frac{\phi}{2}} \right) \frac{\delta}{\xi}\end{aligned}$$



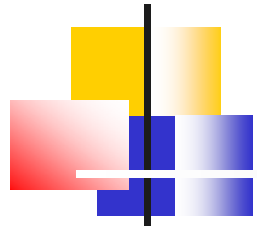
Estimate of Parameter A

➤ Under the Approximation $\delta \doteq x$

$$\varepsilon = \left(1 - \frac{\xi \tan \frac{\phi}{2} - \tan \beta}{R \tan \frac{\phi}{2}} \right) \frac{1}{\xi} x \quad (\equiv Ax)$$

➤ Parameter A

$$A = \left(1 - \frac{\xi \tan \frac{\phi}{2} - \tan \beta}{R \tan \frac{\phi}{2}} \right) \frac{1}{\xi}$$



Newly Developed Simulator

- Magnetic Sector

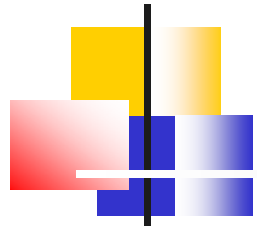
- ✓ Divided into M Small Sub-sectors with Bending Angle

$$\delta\phi = \frac{\phi - 2\beta}{M}$$

- Orbit in Sub-sector

- ✓ Circular Orbit According to Local Field Strength

- 4th Order Runge-Kutta Method



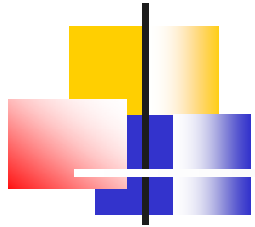
4th Order Runge-Kutta Method

Integration

	Using	To Evaluate
<u>Step.1</u>	$B(s_i, x_i)$	(s_1, x_1, x_1')
<u>Step.2</u>	$B((s_i + s_1)/2, (x_i + x_1)/2)$	(s_2, x_2, x_2')
<u>Step.3</u>	$B((s_i + s_2)/2, (x_i + x_2)/2)$	(s_3, x_3, x_3')
<u>Step.4</u>	$B(s_3, x_3)$	(s_4, x_4, x_4')

$$s_e = \frac{1}{6}(s_1 + 2s_2 + 2s_3 + s_4) \quad , \quad x_e' = \frac{1}{6}(x_1' + 2x_2' + 2x_3' + x_4')$$

$$x_e = \frac{1}{6}(x_1 + 2x_2 + 2x_3 + x_4)$$



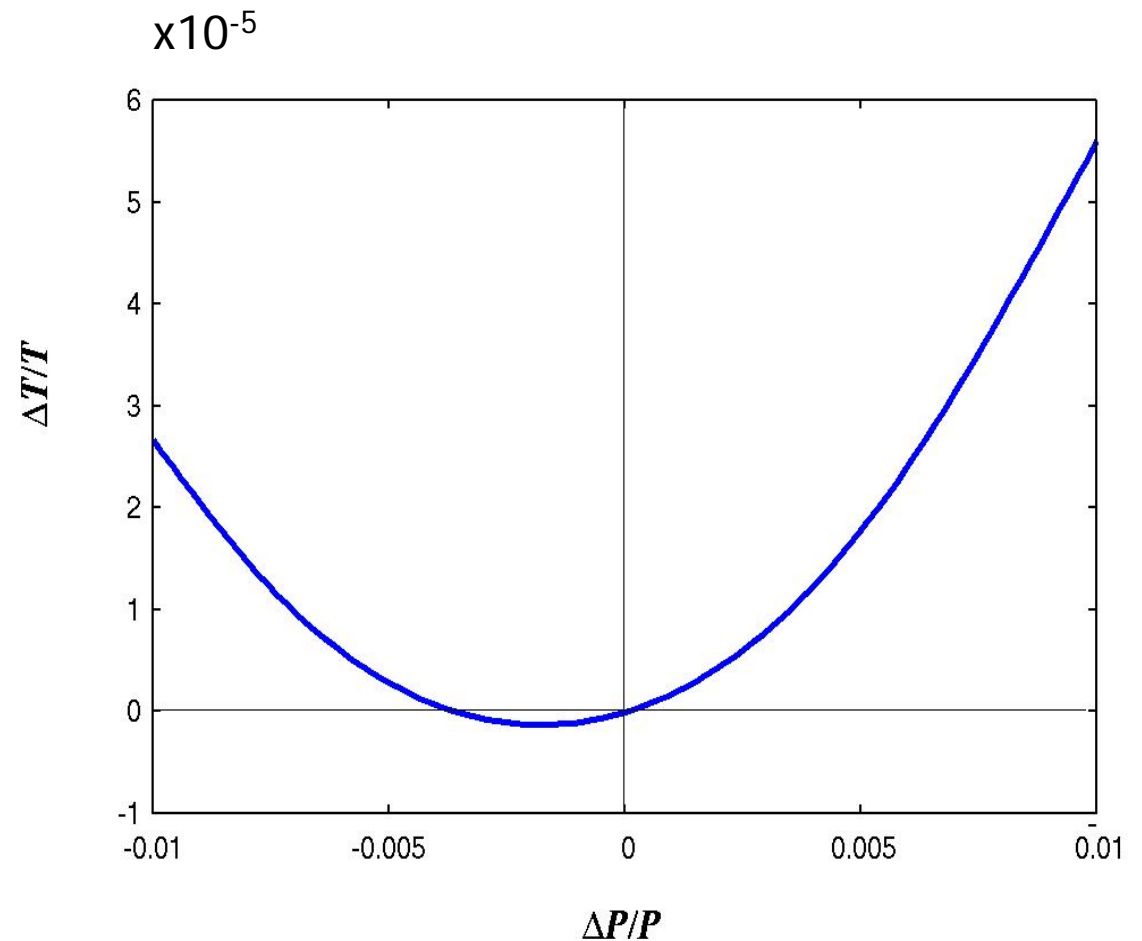
First Order Solution

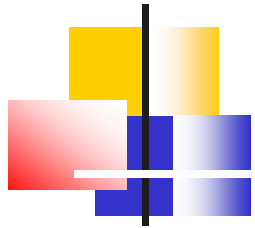
Achieves

$$|\Delta T/T| \leq 6 \times 10^{-5}$$

for

$$|\Delta P/P| \leq 1\%$$





Second Order Solution

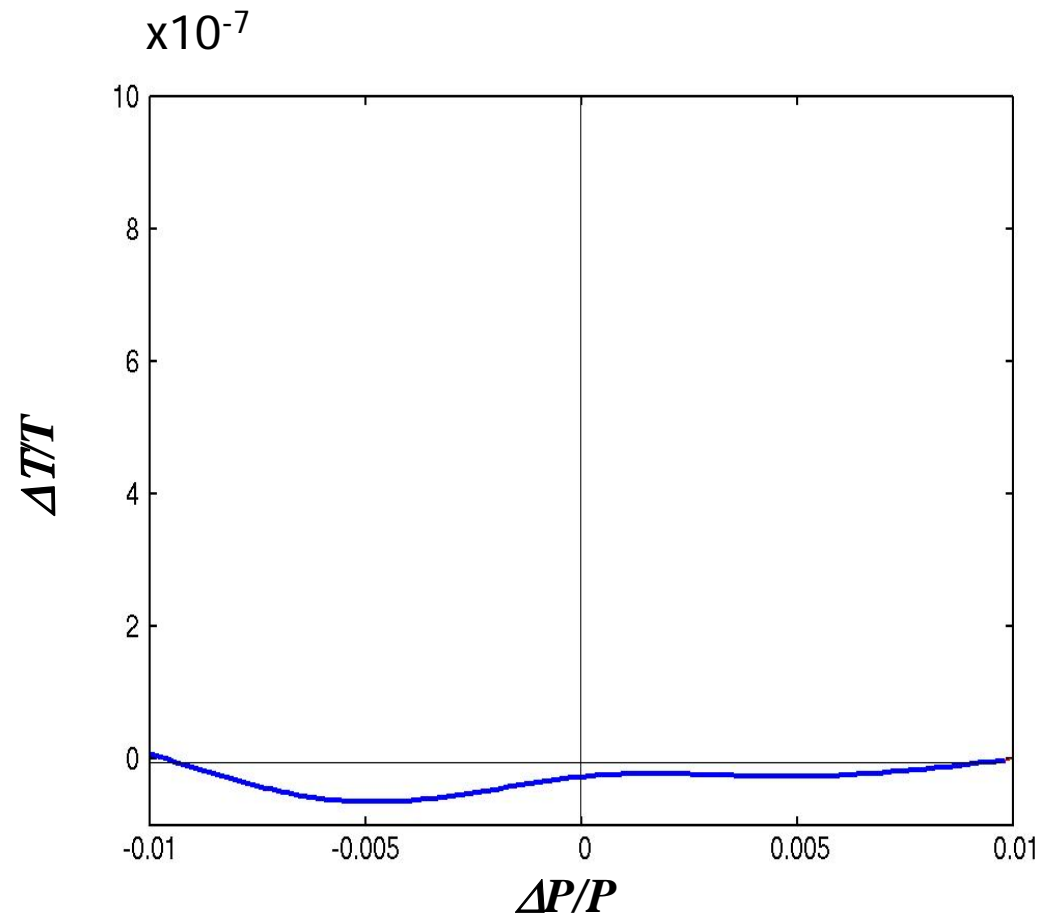
Fine Tuning of A
Determination of B

Achieves

$$|\Delta T/T| \leq 5 \times 10^{-8}$$

for

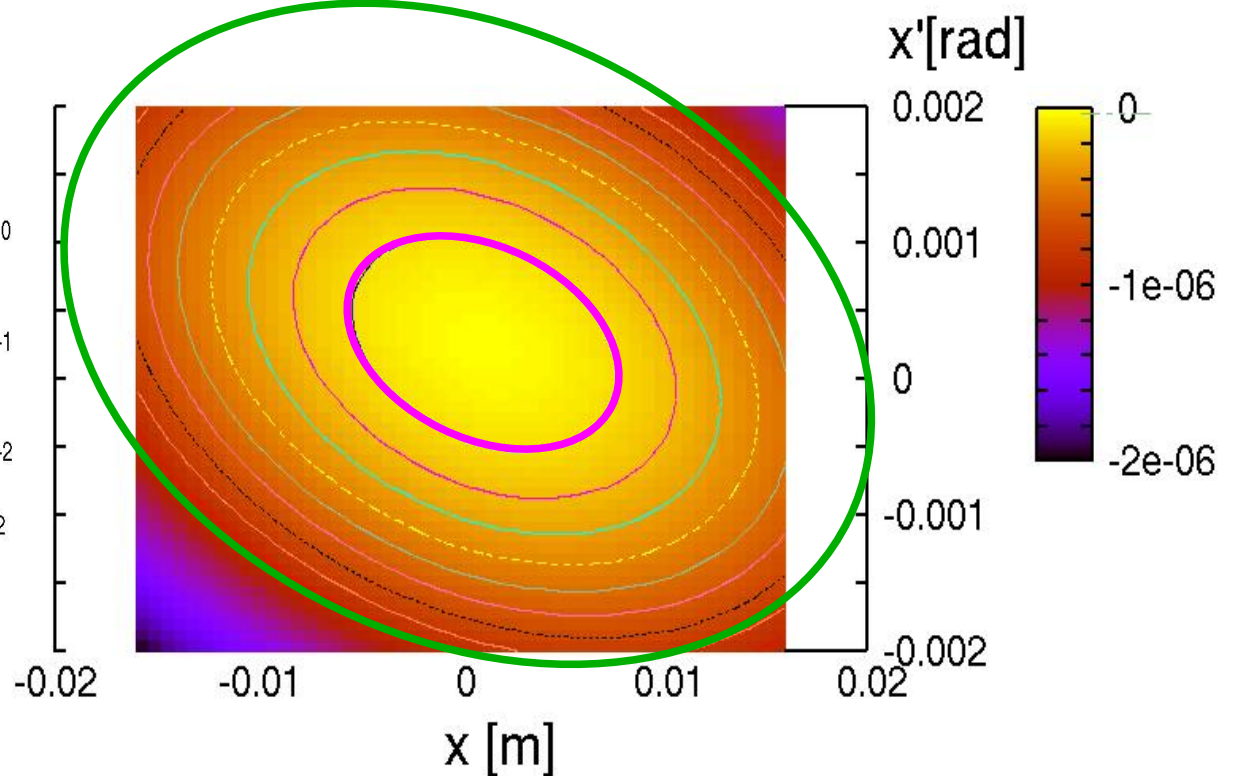
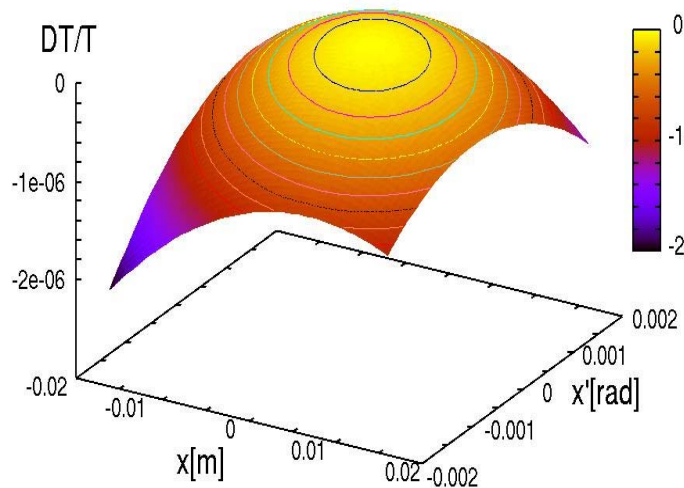
$$|\Delta P/P| \leq 1\%$$

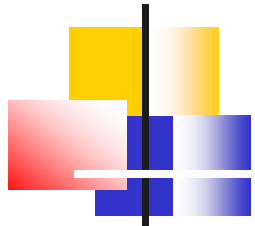


Emittance at $\Delta P/P=0$

➤ 47 [π mm mrad] for $\Delta T/T < 10^{-6}$

➤ 5.2 [π mm mrad] for $\Delta T/T < 10^{-7}$

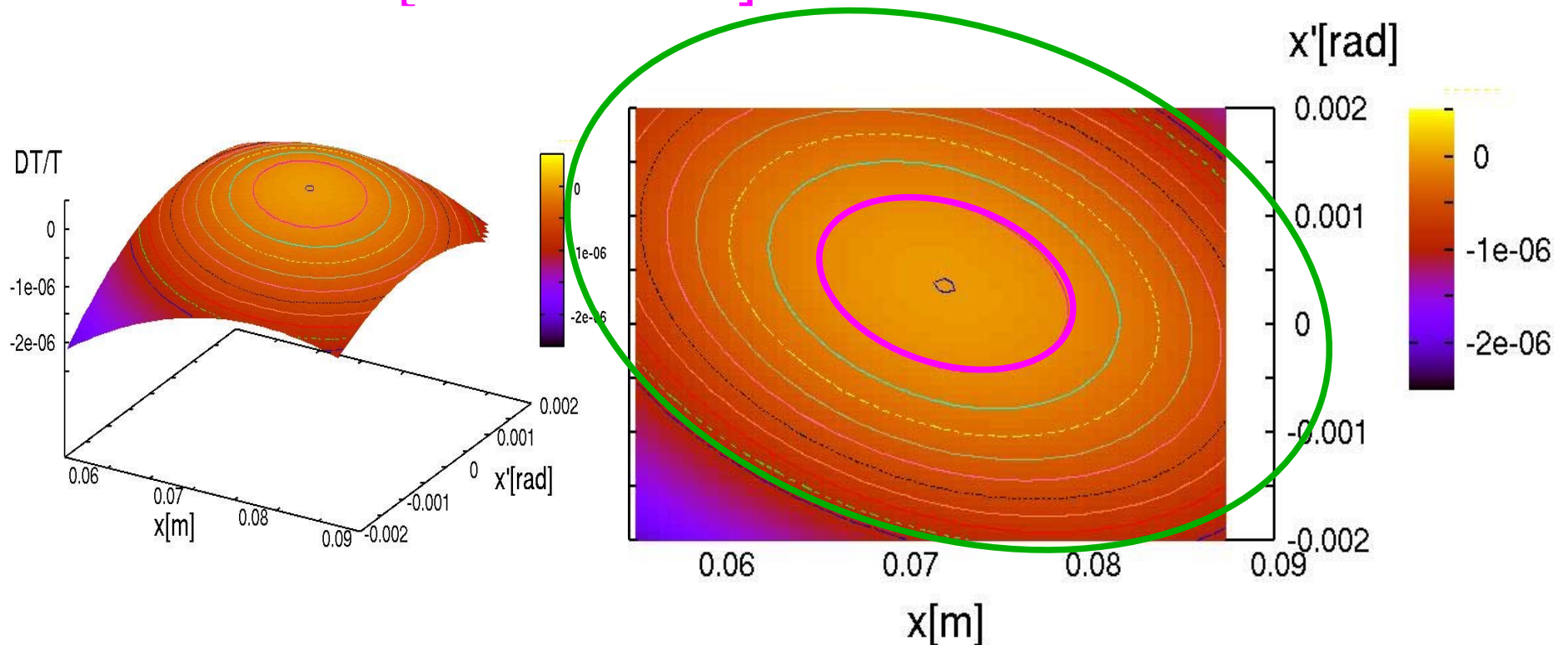


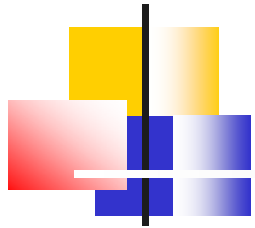


Emittance at $\Delta P/P = +0.01$

➤ 48 [π mm mrad] for $\Delta T/T < 10^{-6}$

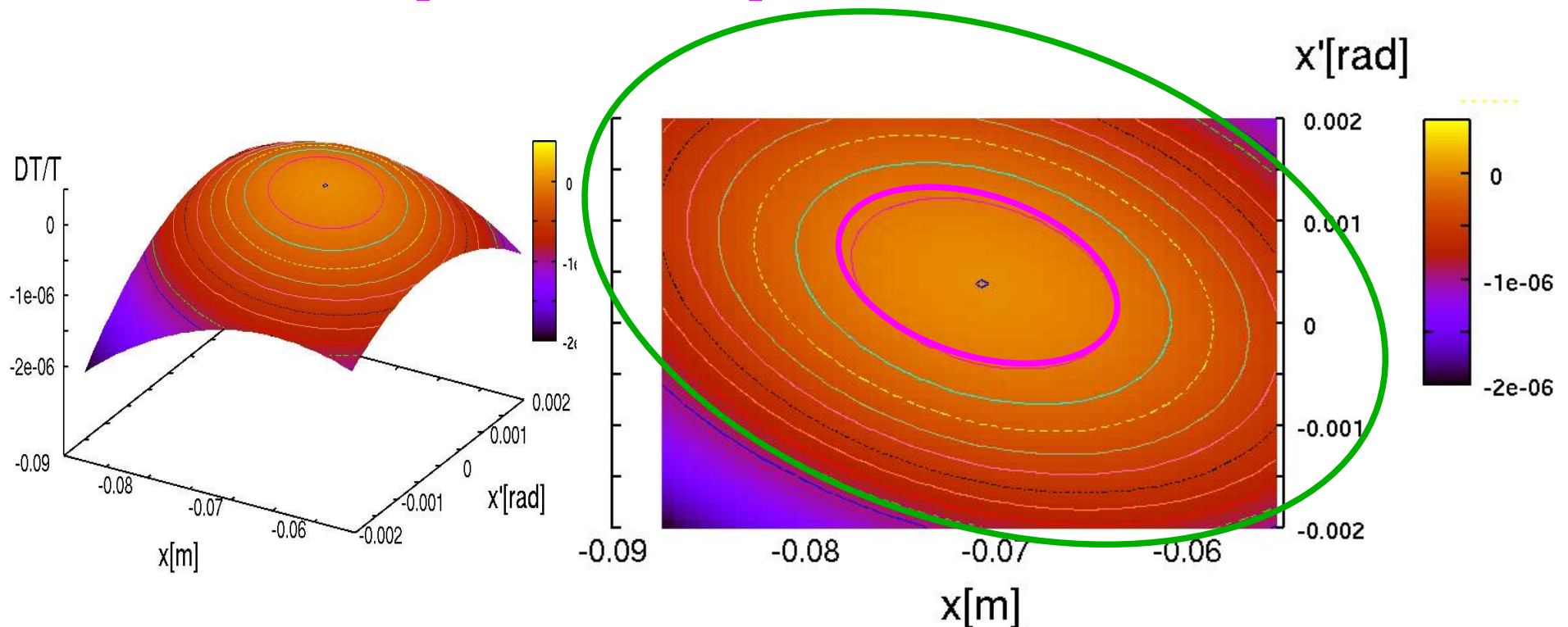
➤ 5.3 [π mm mrad] for $\Delta T/T < 10^{-7}$





Emittance at $\Delta P/P = -0.01$

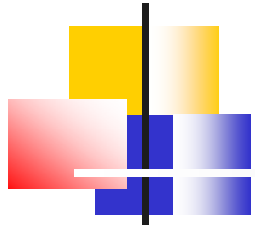
- 49 [π mm mrad] for $\Delta T/T < 10^{-6}$
- 5.6 [π mm mrad] for $\Delta T/T < 10^{-7}$





Emittance -Analytical Evaluation

- After Fine Tuning, Main Contribution for ΔT Comes from Betatron Oscillation
- ΔT is Evaluated by Integrating Flight Length Directly
- Using Different Metrics for
 - ✓ Orbit in Magnetic Sector
 - ✓ Orbit in Straight Section



Betatron Oscillation

➤ Equation of Motion

$$x = a \sin \frac{v_x}{\rho} (s - \delta)$$

$$y = b \sin \frac{v_z}{\rho} (s - \varepsilon)$$

➤ Parameters a , b , δ and ε

✓ Determined by Initial Condition



Metrics for (dx, dy, ds)

➤ Magnetic Sector

$$\begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 + \frac{x}{R} \end{pmatrix}$$

➤ Straight Section

$$\begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$



Flight Length in Magnetic Sector

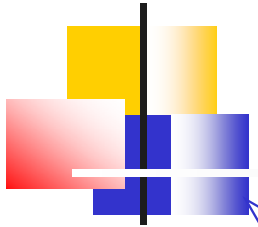
Line Element

$$dl = \sqrt{\left(\frac{dx}{ds}\right)^2 + \left(\frac{dy}{ds}\right)^2 + \left(1 + \frac{x}{\rho}\right)^2} ds$$

Integration up to 2nd Order

$$\int dl \cong \sqrt{1 + \left(\frac{v_x a}{\rho}\right)^2 + \left(\frac{v_y b}{\rho}\right)^2} \int_0^{NL} ds$$
$$+ \frac{1}{2\sqrt{1 + \left(\frac{v_x a}{\rho}\right)^2 + \left(\frac{v_y b}{\rho}\right)^2}} \int_0^{NL} ds \left(-\frac{(1 + v_x^2)x^2 + v_y^2 y^2}{\rho^2} + \frac{2x}{\rho} \right)$$

Flight Length in Straight Section



Line Element

$$dl = \sqrt{\left(\frac{dx}{ds}\right)^2 + \left(\frac{dy}{ds}\right)^2 + 1} ds$$

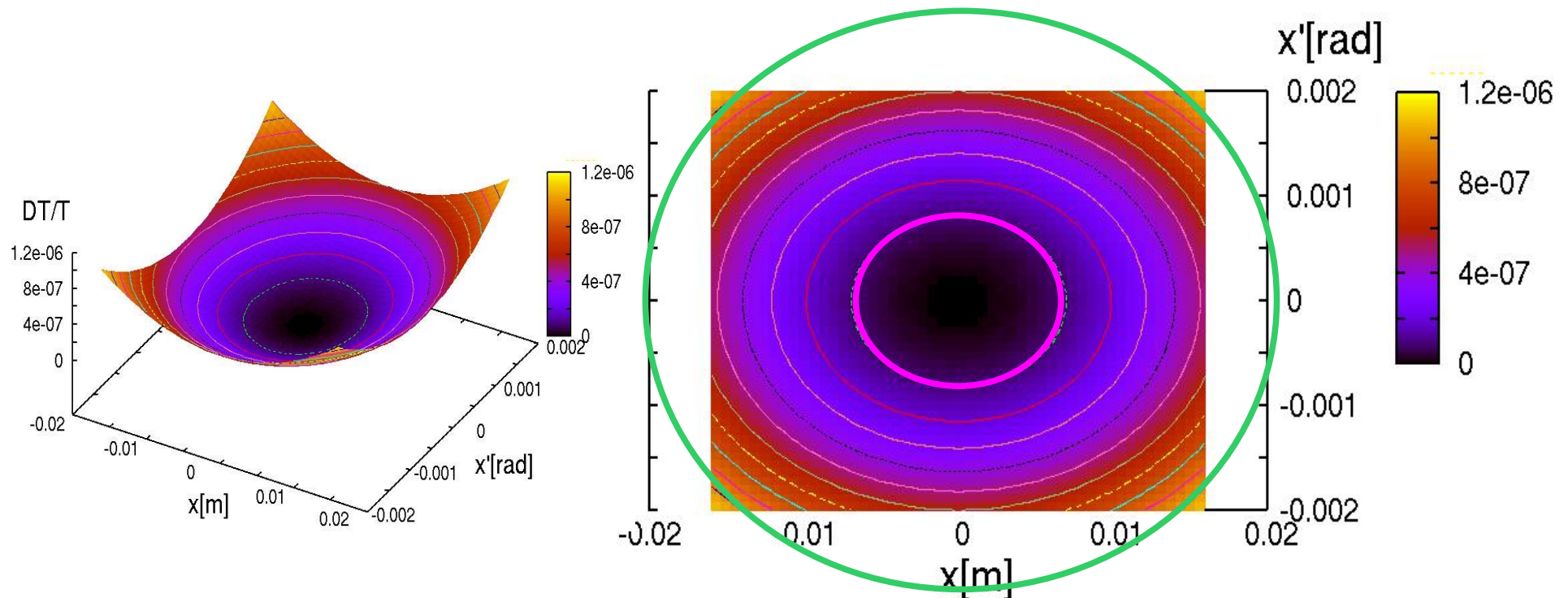
Integration up to 2nd Order

$$\int dl \cong \sqrt{1 + \left(\frac{v_x a}{\rho}\right)^2 + \left(\frac{v_y b}{\rho}\right)^2} \int_0^{NL} ds$$
$$+ \frac{1}{2\sqrt{1 + \left(\frac{v_x a}{\rho}\right)^2 + \left(\frac{v_y b}{\rho}\right)^2}} \int_0^{NL} ds \left(-\frac{v_x^2 x^2 + v_y^2 y^2}{\rho^2} \right)$$

Emittance - Analytical Evaluation

➤ 46 [π mm mrad] for $\Delta T/T < 10^{-6}$

➤ 5.2 [π mm mrad] for $\Delta T/T < 10^{-7}$





Summary

- New Scheme of Precise Mass Measurement
- to Study
 - ✓ Nuclei Far from Stability
 - ✓ Astrophysical r-Process Path
- Preliminary Design Study Shows

Promising!